# Monte Carlo studies of directional pair ordering in disordered binary and ternary ferromagnetic BCC crystalline alloys

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Magnetic field annealing can be used to induce uniaxial magnetic anisotropy in ferromagnetic alloys, which is often desirable, for example, to reduce core losses in materials of interest for high frequency inductive components in power conversion applications. An understanding of the compositional dependence of the uniaxial induced anisotropy constant  $K_U$  is important to develop materials for such applications. In this work, Monte Carlo studies of directional pair ordering in bcc crystalline alloys using the Néel pair model and a Metropolis-type algorithm are reported. The compositional dependence of  $K_U$  in disordered binary alloys is compared with analytical results and extended to the calculation of  $K_U$  for ternary alloys. An approximate  $X_B^2(1-X_B)^2$  functional dependence of  $K_U$  is observed for binary alloys, where  $X_B$  is the atomic fraction of one of the atomic species. For ternary alloys a more complicated functional dependence is observed. These results are used to critically evaluate the potential for increasing  $K_U$  through ternary alloying additions to binary ferromagnetic alloys. © 2007 American Institute of Physics. [DOI: 10.1063/1.2711389]

## INTRODUCTION

The directional pair ordering mechanism of field induced anisotropy first proposed by Néel<sup>1</sup> and investigated in detail by  $Chikazumi^2$  and others<sup>3–5</sup> has been used to explain the composition and temperature dependences of field induced anisotropies in binary ferromagnetic alloys including polycrystalline Ni–Fe.<sup>6,7</sup> Recently, directional pair ordering in a crystalline phase has been used to explain magnetic field induced anisotropy in the Fe-rich (Fe,Co)-based magnetically soft nanocrystalline/amorphous nanocomposite materials such as Finemet and Nanoperm.<sup>8,9</sup> where the crystalline phase is a bcc-derivative structure. To investigate the predictions of Néel's anisotropic pair ordering model for these alloys, Monte Carlo calculations have been used to simulate the formation of an anisotropic distribution of atom pairs in bcc-based binary and ternary ferromagnetic crystalline alloys through magnetic field annealing.

#### MODEL DESCRIPTION AND ASSUMPTIONS

A code using a Metropolis-type<sup>10,11</sup> algorithm, suitable for simulating chemical ordering in binary alloys and considering only nearest neighbor interactions, has been modified to include anisotropic bond energies. A code for use with the commercially available program MATHEMATICA® was written by one of the authors (Ohodnicki). In all simulations, the system Hamiltonian and the transition probability governing the evolution of the ordering during field annealing were

$$E = \frac{1}{2} \sum_{j=1}^{8} \sum_{i=1}^{N} (V_{ij} + \ell_{ij} \cos^2 \theta_j), \qquad (1)$$

$$W = \frac{e^{-(\Delta E^{n \leftrightarrow m}/kT)}}{\left[1 + e^{-(\Delta E^{n \leftrightarrow m}/kT)}\right]},\tag{2}$$

where the sums with *i* and *j* indices are taken over the atomic positions in the simulated crystals and the eight possible near neighbor directions, respectively. E is the overall bond energy of the crystal, including both isotropic  $(V_{ii})$  and anisotropic  $(\ell_{ii})$ 's) contributions.  $\Delta E^{n \leftrightarrow m}$  is the change in internal energy associated with swapping the atom at the nth lattice position and the mth lattice position. W is a transition probability<sup>10</sup> calculated using  $\Delta E^{n \leftrightarrow m}$ . The magnetization is assumed to be saturated along a particular direction, and  $\theta_i$  is the angle between the assumed magnetization direction and the *j*th bond direction.  $V_{ii}$  and  $\ell_{ii}$ , respectively, are the isotropic bond energy and anisotropic pseudodipolar interactions between the atom at the *i*th position and the nearest neighbor atom oriented along the *j*th bond direction. The inclusion of both chemical and pseudodipolar nearest neighbor interactions between atoms for long-range and shortrange chemical ordering and anisotropic directional pair ordering in binary alloys has been carried out by Iwata in a statistical mechanics framework using the Bethe approximation.<sup>12</sup> This work motivated our choice of the Hamiltonian of Eq. (1), although here the isotropic part of the pseudodipolar contribution is absorbed into the  $V_{ii}$ 's.

In all simulations, a disordered binary or ternary crystal of  $16 \times 16 \times 16$  conventional unit cells (9826 atoms) was generated on a bcc lattice with a specified composition. Simulated field annealing was carried out at a fixed temperature by choosing a magnetization orientation and a corresponding set of  $\ell_{ij}$ 's and  $V_{ij}$ 's. Using the pseudorandom number generator function in MATHEMATICA®, pairs of atoms were chosen randomly, and the values of  $\Delta E^{n \leftrightarrow m}$  and W were calculated. Atoms were swapped if W was larger than a random number generated between 0 and 1. Periodic boundary conditions were employed. Attention is focused here on ideal

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FIG. 1. (Color online) (a) Induced anisotropy constant  $(K_U)$  as a function of composition for an ideal binary solid solution and (b) as a function of annealing temperatures illustrating agreement with the expected compositional and temperature trend. The plotted points are actual simulation results, while the curves are fitted to  $K_U \propto X_B^{-2}(1-X_B)^2$  and  $K_U \propto 1/(kT_{anneal})$ , respectively.

solid solutions where the  $V_{ii}$ 's are all equal and/or zero.

Most simulations were carried out for  $\sim 10^6$  attempted atomic swaps, though several longer simulations ( $\sim 10^7$ ) were conducted to verify that a metastable state was not approached. The magnitude of the induced anisotropy was calculated according to the following expression ( $M_{\text{anneal}}$  corresponds to the magnetization direction assumed during annealing):

$$K_{U} = \left[ \frac{1}{2} \sum_{j=1}^{8} \sum_{i=1}^{N} (\ell_{ij} \cos^{2} \theta_{j}) \right] \Big|_{M \perp M_{\text{anneal}}} - \left[ \frac{1}{2} \sum_{j=1}^{8} \sum_{i=1}^{N} (\ell_{ij} \cos^{2} \theta_{j}) \right] \Big|_{M \parallel M_{\text{anneal}}}.$$
 (3)

Equation (3) is only truly valid in the case where  $M_{\text{anneal}}$  is along one of the high symmetry directions of the cubic crystal; otherwise the induced easy axis is expected to deviate from the direction of  $M_{\text{anneal}}$ .

### **DISCUSSION OF MODEL RESULTS**

Figure 1(a) plots values of  $K_U$  calculated according to Eq. (3) as a function of the composition for a binary alloy using:

$$\frac{\ell_{AB}}{kT_{\text{anneal}}} = -\frac{\ell_{AA}}{kT_{\text{anneal}}} = -\frac{\ell_{BB}}{kT_{\text{anneal}}} = \frac{\ell}{kT_{\text{anneal}}} = -0.1.$$
(4)

The magnetization was assumed to be oriented along [111], which results in the maximum  $K_U$  for binary bcc single crystals according to directional pair ordering theory.<sup>2,12</sup> For the chosen parameters of Eq. (4), the composition dependence of  $K_U$  for a binary ideal solid solution is well fitted to Iwata's expression  $K_U \propto X_B^{-2}(1-X_B)^{2}$ .<sup>12</sup> Because  $\ell_{ij}/kT \ll 1$  is typically true for realistic annealing temperatures, care must be taken in choosing the values of  $\ell_{ij}$  to be significantly less than  $kT_{\text{anneal}}$  to obtain good agreement with experiment and Iwata's theory. Actually, the necessary condition for a binary alloy is  $\ell_0^{-AB}/kT \ll 1$  for all  $\ell_{ij}$ 's implies  $\ell_0^{-AB}/kT \ll 1$ . For smaller assumed values of  $\ell_{ij}/kT$ ,  $K_U$  values are more difficult to estimate reproducibly since the fluctuations in  $K_U$  become comparable to the magnitude of  $K_U$ . Values of

 $\ell_{ij}/kT_{\text{anneal}}$  were chosen according to Eq. (4), so that the model reasonably reproduced the expected variation of  $K_U$  in the binary system without making estimation of the  $K_U$  value prohibitively difficult.

The extended model has also been used to investigate the dependence of  $K_U$  on the annealing temperature with fixed values of  $\ell_{ij}$ . Here, the values of  $\ell_{ij}$  were assumed independent of temperature (a good approximation for alloys with  $T_{\text{Curie}} \gg T_{\text{anneal}}$ ), and  $K_U$  is expected to vary as  $K_U$  $\propto 1/(kT_{\text{anneal}})$  if the expression  $\ell_{ij}/kT \ll 1$  holds.<sup>2,12</sup> Figure 1(b) shows that the observed values of  $K_U$  for several compositions of the binary alloy using the  $\ell_{ij}$ 's of Eq. (4) are well fitted by expressions of this form.

The model was extended to an ideal ternary solid solution where four additional  $\ell_{ij}$ 's are required to specify the interactions of the system. To include isotropic chemical interactions. For binary alloys, the development of  $K_U$  is governed entirely by a single parameter defined by Eq. (5), which is analogous to the well-known chemical interaction parameter:

$$V^{AB} = V_{AB} - \frac{1}{2}(V_{AA} + V_{BB}),$$
  
$$\ell_0^{AB} = \ell_{AB} - \frac{1}{2}(\ell_{AA} + \ell_{BB}).$$
 (5)

A positive or negative  $V^{AB}$  indicates a tendency for formation of less or more AB pairs, respectively, as compared to an ideal solid solution. The generalization to anisotropic bond energies predicts AB pairs to orient parallel to the magnetization direction during annealing for a binary alloy when  $\ell_0^{AB}$  is negative. When  $\ell_0^{AB}$  is positive, AA and BB pairs tend to orient parallel to the magnetization direction. If  $\ell_0^{AB}$ does not change sign between measurement and annealing temperatures, the induced easy axis lies along the magnetization direction during annealing if it is a high symmetry direction of the crystal.  $K_U$  is expected to increase monotonically up to  $X_B=0.5$  following the relationship  $K_U \propto X_B^2(1 - X_B)^2$ . These predictions are independent of the absolute and relative values of  $\ell_{AA}$ ,  $\ell_{BB}$ ,  $\ell_{AB}$ , and hence  $\ell_0^{AB}$ , though the magnitude of  $K_U$  does depend on the magnitude of  $\ell_0^{AB}$ .

Figure 2 represents a binary crystal, a (110) planar section, and the magnetic anisotropy energy surface (neglecting magneto-crystalline anisotropy) for the parameters chosen in Eq. (4)  $(\ell_0^{AB}/kT_{anneal}=-2\ell=-0.2)$  and also after replacing  $\ell$ with  $-\ell$   $(\ell_0^{AB}/kT_{anneal}=+0.2)$  for comparison. Since the predicted compositional dependence of  $K_U$  does not depend on the values of the  $\ell_{ij}$  parameters, a common technique used to increase field induced anisotropy in ferromagnetic materials has been to add a second ferromagnetic transition metal element to allow directional pair ordering between the atomic species  $(K_U \propto X_B^2$  for dilute binary alloys).<sup>9</sup>

In ternary alloys, one can define an  $\ell_0$  parameter for each of the unlike bonds ( $\ell_0^{AB}$ ,  $\ell_0^{AC}$ , and  $\ell_0^{BC}$ ) and several new configurations can arise. Thus, the analysis is more complicated and the compositional dependence of  $K_U$  is a richer problem than for the corresponding binary alloys. To investigate these compositional effects, two different sets of  $\ell_{ij}$ 's were used. The first set is chosen to be the same as the parameters used in Eq. (4) to generate Fig. 1. These param-



FIG. 2. (Color online) Graphical illustrations of binary bcc crystals and corresponding (110) sections and magnetic anisotropy energy surfaces (neglecting magnetocrystalline) after simulated field annealing for  $\ell_0^{AB}$  = +0.2 $kT_{\rm anneal}$  (top row) and  $\ell_0^{AB}$  = -0.2 $kT_{\rm anneal}$  (bottom row).

eters are listed in Eq. (6) and result in values of  $\ell_0^{AB}$ ,  $\ell_0^{AC}$ , and  $\ell_0^{BC} = -0.2kT_{\text{anneal}}$ . Here all unlike atom pairs prefer to lie parallel to the magnetization, and the same composition dependence of  $K_U$  is expected in the corresponding binary systems,

$$\frac{\ell_{AB}}{kT_{\text{anneal}}} = \frac{\ell_{AC}}{kT_{\text{anneal}}} = \frac{\ell_{BC}}{kT_{\text{anneal}}} = \frac{\ell}{kT_{\text{anneal}}} = -0.1,$$
$$\frac{\ell_{AA}}{kT_{\text{anneal}}} = \frac{\ell_{BB}}{kT_{\text{anneal}}} = \frac{\ell_{CC}}{kT_{\text{anneal}}} = -\frac{\ell}{kT_{\text{anneal}}} = +0.1.$$
(6)

A second set of parameters assumed  $\ell_{BC}/kT_{\text{anneal}} = +0.15$  with all other interaction parameters defined as in Eq. (6). Here the magnitudes of the  $\ell_0^{AB}$ ,  $\ell_0^{AC}$ , and  $\ell_0^{BC}$  parameters are identical, but the *B*-*C* pairs would prefer to lie perpendicular to the magnetization direction in the corresponding binary alloy while the *A*-*B* and *A*-*C* pairs prefer to lie parallel  $(\ell_0^{AB} = \ell_0^{AC} = -0.2kT_{\text{anneal}})$  and  $\ell_0^{BC} = +0.2kT_{\text{anneal}})$ .

 $K_U$  versus composition for three pseudobinary systems corresponding to different fixed atomic ratios of A:B (50:50, 70:30, and 90:10) is shown in Fig. 3. The variation with addition of a ternary alloying element is more complicated, and even the qualitative variation of  $K_U$  depends on the interaction parameters in the system.  $K_U$  decreases with addition of element C to the 50:50 and 70:30 pseudobinary systems for the first parameter set.  $K_U$  increases for all



FIG. 3. (Color online)  $K_U$  as a function of addition of ternary alloying element *C* to a binary alloy of fixed *A*:*B* atomic ratio for (a)  $\ell_0^{AB} = \ell_0^{AC} = \ell_0^{BC} = -0.2kT_{\text{anneal}}$  and (b)  $\ell_0^{AB} = \ell_0^{AC} = -\ell_0^{BC} = -0.2kT_{\text{anneal}}$ . In all cases the predicted values of  $K_U$  for each of the binary systems are identical according to directional pair ordering theory.

pseudodobinaries presented with addition of element *C* for the second parameter set. For both parameter sets,  $K_U$  increases with *C* content for the 90:10 pseudobinary. This result is reasonable as in the dilute limit of both the second and third elements, the binary alloy relationship  $K_U \propto (X_C^2)$  is expected due to the low probability of interacting *B*-*C* pairs. According to these results, one should not necessarily expect  $K_U$  to increase in proportion to  $X_C^2$  unless the solid solution is dilute in both the second and third alloying elements. In ternary alloys, where the field induced anisotropy is primarily due to directional pair ordering, prediction of the variation in  $K_U$  with third element alloying additions is not so straightforward and the strategy to increase  $K_U$  is not obvious without detailed information regarding the system's interaction parameters.

#### CONCLUSIONS

Monte Carlo simulations reproduce results of the Neél theory of directional pair ordering during magnetic field annealing for ideal binary alloys. The extension to ternary systems shows that even for an ideal ternary solid solution,  $K_{II}$ does not necessarily increase with ternary element alloying additions. Unlike the case for binary alloys, the variation of  $K_U$  with atomic fraction of a third alloying element depends on the relative values of  $\ell_{ii}$ 's in the system. However, when both the second (element B) and third (element C) alloying elements are dilute, the compositional dependence of  $K_U$  is still expected to vary as  $K_U \propto X_C^2$  because of the low probability of finding B-C pairs in the alloy. We conclude that the common strategy of adding an additional atomic species to enable directional pair ordering through formation of a binary alloy does not straightforwardly extend to the general ternary case.

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