

Solutions to Set #11, 24-26, Fall 2001
1. (3, 7-9)

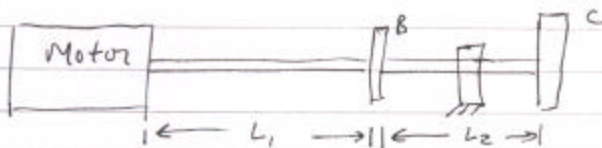
Motor delivers 275 hp at 1000 rpm

Find torque delivered by motor

$$\text{Power} = 275 \text{ hp} = 275(550) \frac{\text{ft-lb}}{\text{s}} = 151 \times 10^3 \frac{\text{ft-lb}}{\text{s}}$$

$$1000 \text{ rpm} = 1000 \frac{2\pi \text{ rad}}{\text{rot}} \frac{1 \text{ min}}{60 \text{ s}} = 104.7 \text{ rad/s}$$

$$\text{Since } P = T\omega \Rightarrow T = \frac{P}{\omega} = \frac{151 \times 10^3}{104.7} = 1444 \text{ ft-lb}$$

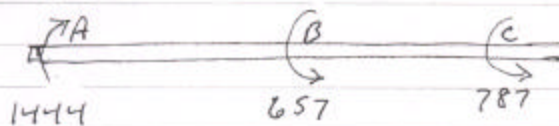


Since whole shaft has $\omega = 104.7 \text{ rad/s}$,
if gears B & C deliver 125 and 150 hp, respectively

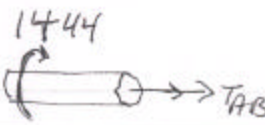
$$\text{They apply torques of } T_B = \frac{(125)(550)}{104.7} = 657 \text{ ft-lb}$$

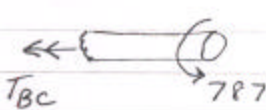
$$\text{and } T_C = \frac{(150)(550)}{104.7} = 787 \text{ ft-lb}$$

Look at shaft



shaft is running at constant speed; it is
in equilibrium (torques balance)

In AB  $T_{AB} = 1444$

In BC  $T_{BC} = 787$

Max shear stress is in AB (T is max there and cross-section is uniform)

$$\tau_{max} = \frac{T r}{I_p} = \frac{T r}{\frac{\pi}{2} r^4} = \frac{2T}{\pi r^3}$$

$$\frac{2T}{\pi r^3} < 7500 \Rightarrow r > \left[\frac{2T}{\pi(7500)} \right]^{1/3} = \left[\frac{2(1444)(12)}{\pi(7500)} \right]^{1/3}$$

$$r > 1.137''$$

$$\text{Total angle of twist} = \Delta\phi_{AB} + \Delta\phi_{BC} < 1.5^\circ$$

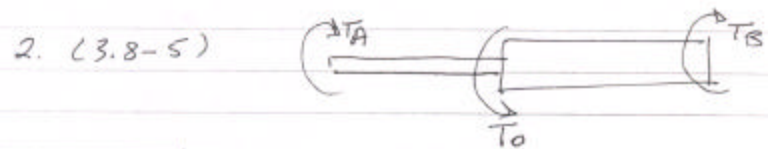
$$\frac{T_{AB} L_1}{G I_p} + \frac{T_{BC} L_2}{G I_p} < 1.5^\circ \Rightarrow (1444)(6)(12)^2 + (787)(4)(12)^2 < 1.5 \left(\frac{\pi}{180} \right) (11.5 \times 10^6) \frac{\pi}{2} r^4$$

$$\Rightarrow r > 1.377''$$

Both conditions must be satisfied

r must be greater than maximum

$$\Rightarrow \boxed{d > 2.75''}$$



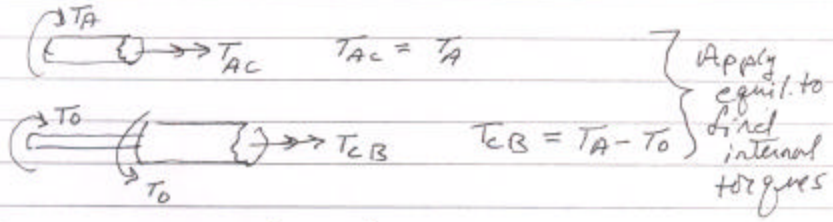
$$\sum M_x = T_0 - T_A - T_B = 0 \Rightarrow T_A + T_B = T_0 \quad \text{static.}$$

Know that ends A & B are fixed $\Rightarrow \phi_A = \phi_B = 0$

twist of AB = $\phi_C - \phi_A \Rightarrow \Delta\phi_{AC} = \phi_C$ ($\phi_A = 0$)

twist of CB = $\phi_B - \phi_C \Rightarrow \Delta\phi_{CB} = -\phi_C$ ($\phi_B = 0$)

So twists are related $\Delta\phi_{AC} = -\Delta\phi_{CB}$



Apply torque-twist relation

$$\Delta\phi_{AC} = \frac{T_{AC} L_{AC}}{G J_{PAC}} \quad \Delta\phi_{CB} = \frac{T_{CB} L_{CB}}{G J_{PCB}}$$

$$J_{PAC} = \frac{\pi}{2} (0.4)^4 \quad J_{PCB} = \frac{\pi}{2} (0.8)^4$$

$$\Delta\phi_{AC} = -\Delta\phi_{CB} \Rightarrow \frac{T_A (8)}{(0.4)^4} = -\frac{(T_A - T_0)(20)}{(0.8)^4}$$

$$T_A (8)(2)^4 = (T_0 - T_A)(20) \Rightarrow T_A = \frac{20 T_0}{20 + 8(16)}$$

$$\text{or } T_A = 0.135 T_0$$

$$T_A + T_B = T_0 \Rightarrow T_B = 0.865 T_0$$

Consider max shear stress in each

$$(\tau_{max})_{AC} = \frac{|T_{AC}| r_{AC}}{\frac{\pi}{2} (r_{AC})^4} \Rightarrow \frac{2(0.135)T_0}{\pi(0.4)^3} = 1.343 T_0$$

$$(\tau_{max})_{CB} = \frac{|T_{CB}| r_{CB}}{\frac{\pi}{2} (r_{CB})^4} = \frac{2(0.865)T_0}{\pi(0.8)^3} = 1.076 T_0$$

so max shear is in AC

$$1.343 T_0 = 8000 \text{ psi} \Rightarrow T_0 = 5960 \text{ lb-in}$$

$$\Rightarrow T_B = 0.865 T_0 = 5150 \text{ lb-in}$$

In CB, the stress is governed by $|T_{CB}|$

$$\tau = \frac{T r}{I_p} = \frac{(5150)(0.5)}{\frac{\pi}{2} (0.8)^4} = 4000 \text{ psi}$$

$\tau = 4000 \text{ psi}$ at a radial position
of 0.5" from center-line
in the segment CB

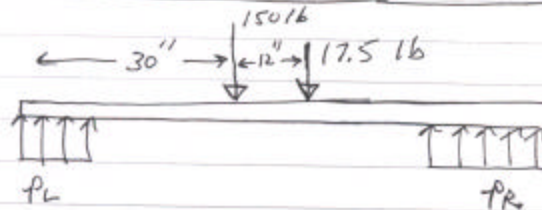
$$(\varphi_B - \varphi_0) = \frac{TL}{GI_p} = \frac{(-5150)(10)}{(11 \times 10^6) \frac{\pi}{2} (0.8)^4} = -7.28 \times 10^{-3}$$

since $\varphi_B = 0$ $\varphi_0 = 7.28 \times 10^{-3} \text{ rad} = 0.417^\circ$

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$$\text{Weight of board} = \left(40 \frac{\text{lb}}{\text{ft}^3}\right) \left(\frac{1\text{ft}}{12\text{in}}\right)^3 (84)(0.75)(12)$$

$$W = 17.5 \text{ lb}$$

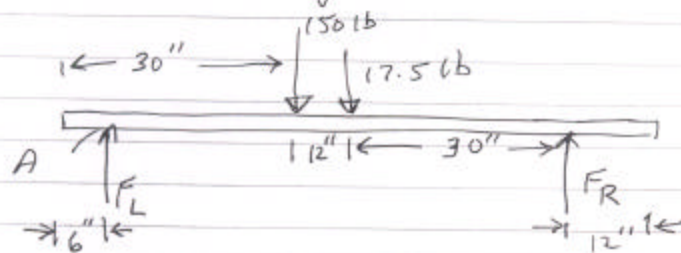


17.5 acts
at midpoint
of beam
(since we
only want
net force
& moment
to be right)

pressures are uniform \Rightarrow replace by

pressure times area acting in middle.

since we are only interested in net force & moment




$$\sum M|_{A_2} = (-150)(24) - (17.5)(36) + F_R(66) = 0$$

$$F_R = 64.1 \text{ lb}$$

$$\sum F_y = F_L + F_R - 150 - 17.5 = 0 \Rightarrow F_L = 103.4 \text{ lb}$$

$$P_L = \frac{103.4}{(12)(12)} = 0.718 \text{ psi} \quad P_R = \frac{64.1}{(12)(24)} = 0.223 \text{ psi}$$

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$$g(x) = 50 \frac{x}{9}$$

Force acting on dx is $g(x)dx = 50 \frac{x}{9} dx$

(ii) Net force = $\int_0^9 50 \frac{x}{9} dx = 50 \frac{x^2}{18} \Big|_0^9$
 $= 225 \text{ N}$

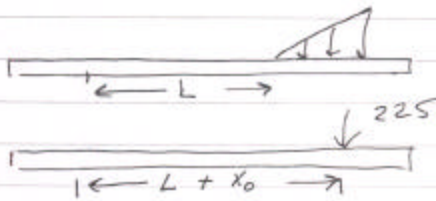
(iii) Net moment is found from adding contribution of each dx to m/z

$$\frac{(L+x)g(x)dx}{\text{moment arm} \quad \text{force}}$$

$$\text{Net moment} = \int_0^9 [L+x] 50 \frac{x}{9} dx$$

$$= 50L \frac{x^2}{18} \Big|_0^9 + \frac{50x^3}{27} \Big|_0^9 = 225L + 1350 \text{ N}$$

(iii)



$$(L+x_0)(225) = 225L + 225x_0 = 225L + 1350$$

$$\Rightarrow x_0 = 6 \text{ cm}$$

So force is to be applied at $x = 6 \text{ cm}$.

This $\frac{2}{3}$ of way from beginning of distribution to the end.

$$\begin{aligned}
 F_t &= 100 \cos 30^\circ - F_A - F_B \\
 &= 100 \cos 30^\circ - \mu_k (N_A + N_B) \\
 &= 100 \cos 30^\circ - \mu_k (10) [17 - 4 \mu_k]
 \end{aligned}$$

$$(a) \mu_k = 0 \Rightarrow F_t = 100 \cos 30^\circ = 86.6 \text{ lb}$$

$$(b) \mu_k = 0.1 \Rightarrow F_t = 70 \text{ lb}$$

if sleeve is thicker, then the forces N_A & N_B would be smaller. Hence F_t would be closer to $100 \cos 30^\circ$

if sleeve is thinner, N_A & N_B would be larger. F_t would even less compared to $100 \cos 30^\circ$