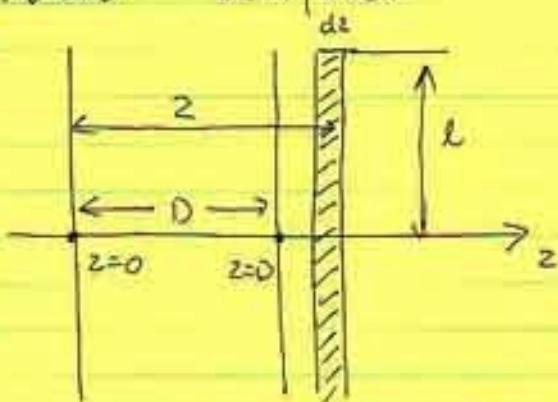


Contact mechanics and adhesion

- Surface and adhesion forces
- Derjaguin approximation
- Indentation forces

Consider the energy per unit area in the interaction of two planar surfaces



Using the earlier derived potential for the interaction between molecule and surface

$$W(D) = -2\pi C S / ((n-2)(n-3) D^{n-3})$$

For a thin sheet of molecules with unit area and thickness d_2 , at a distance z away from another surface (of large area), the interaction energy is :

$$w(z) = -\underbrace{2\pi C g}_{\text{interaction energy for a sheet of unit area}} \underbrace{(z d_2)}_{\text{number of molecules in a sheet of unit area and thickness } d_2} / (n-2)(n-3) z^{n-3}$$

interaction energy for a sheet of unit area number of molecules in a sheet of unit area and thickness d_2

For two surfaces (integration over all sheets d_2) :

$$w(D) = -\frac{2\pi C g^2}{(n-2)(n-3)} \int_0^\infty \frac{d_2}{z^{n-3}} = -\frac{2\pi C g^2}{(n-2)(n-3)(n-4)} D^{n-4}.$$

For $n=6$

$$w(D) = -\pi C g^2 / 12 D^2 \quad \text{per unit area!}$$

Interaction energy per unit area for two planar surfaces can be used to describe the ear interaction force between macroscopic bodies.

Consider the force between sphere and flat surface:

$$F(D) = - \frac{\partial w(D)}{\partial D} = - \frac{4\pi^2 C \rho^2 R}{(n-2)(n-3)(n-4) D^{n-4}}$$

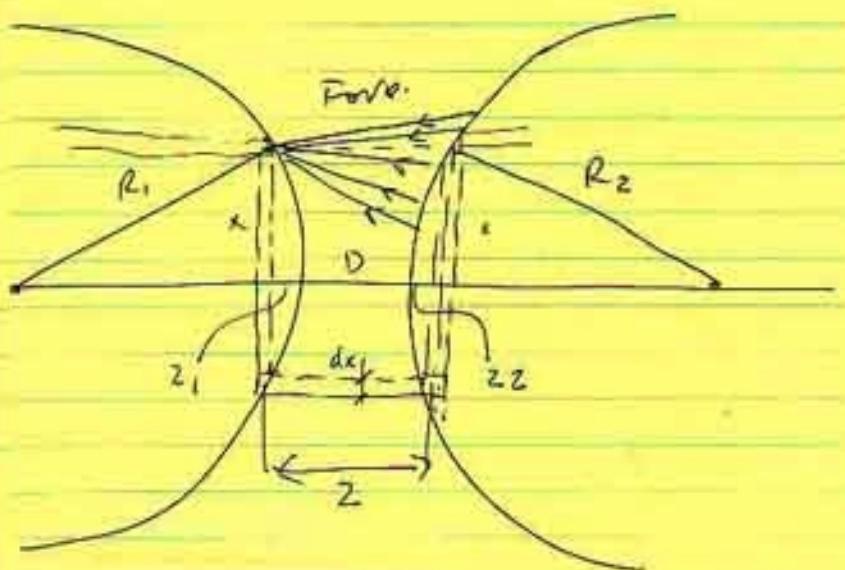
Compare with

$$F(D)_{\text{sphere}} = 2\pi R \underbrace{w(D)}_{\substack{\text{planes} \\ \text{per unit area}}}.$$

So far, we have dealt only with additive potentials $w(r) = -C/r^n$.

The obtained relationship is however valid for any type of force law.

Consider two large spheres of radii R_1 and R_2 , separated by small distance D



If $R_1 \gg D$ and $R_2 \gg D$, the force between the spheres can be obtained by integrating the force between the small circular regions $2\pi \times dx$ as shown above

$$F(D) = \int_{z=0}^{z=\infty} 2\pi \times dx \cdot f(z)$$

$f(z)$: normal force per unit area between two flat surfaces.

using chord theorem
 $x^2 \approx 2R_1 z_1 = 2R_2 z_2$

$$z = D + z_1 + z_2 = D + \frac{x^2}{2} \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$$

thus:

$$dz = \left(\frac{1}{R_1} + \frac{1}{R_2} \right) \times dx$$

and

$$F(D) \approx \int_D^\infty 2\pi \left(\frac{R_1 R_2}{R_1 + R_2} \right) f(z) dz =$$

$$= 2\pi \left(\frac{R_1 R_2}{R_1 + R_2} \right) W(D)$$

Notice: independent of the type of potential we use!

energy per unit area for two surfaces at separation D

Derjaguin approximation.

Valid for any force law, provided that the separation distance D , is much larger than the radius of the spheres.

Some special cases :

- $R_2 \gg R_1$,

$$F(0) = 2\pi R_1 W(D)$$

the same as

- $R = R_1 = R_2$ (two equal spheres).

$$F(D) = \pi R W(D).$$

- two spheres in contact ($D = d$)

the value of $W(d) \rightarrow$
can be associated with the
surface free energy per unit
area of the surface γ

$$W(d) = 2\gamma$$

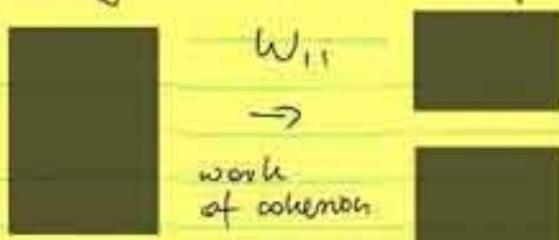
$$F(d) = F_{ad} = \frac{4\pi \gamma R_1 R_2}{R_1 + R_2}$$

↑

adhesion force between two
spheres.

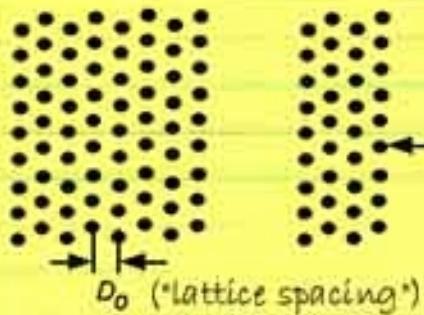
Surface free energy

Consider the cost of separating a body into two pieces



$$\gamma_1 = \frac{1}{2} w_{11} \quad \text{surface free energy (per unit area)}$$

We can calculate w_{11} (and thus γ_1) based on our simple pairwise summation of interaction energies between identical media.



$$w = -A/(2\pi D^2)$$

Work required to separate two pieces by D :

$$\Delta w = \frac{A}{12\pi D_0^2} \left(\frac{1}{D_0^2} - \frac{1}{D^2} \right) =$$
$$= \frac{A}{12\pi D_0^2} \left(1 - \frac{D_0^2}{D^2} \right)$$

Separation to infinity $D = \infty$

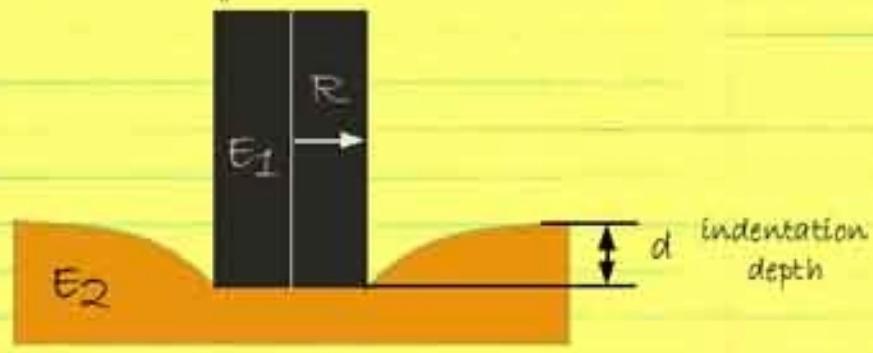
$$\Delta w = w_{11} = \frac{A}{12\pi D_0^2} = 2\gamma$$

$$\gamma = \frac{A}{24\pi D_0^2}$$

Surface free energy
as a function of Hamaker constant!

Indentation

flat cylindrical indenter



E_1, E_2 - Sample and indenter

Young's moduli

R - indenter radius.

ν_1, ν_2 - Poisson coefficients

for $E_2 \gg E_1$,

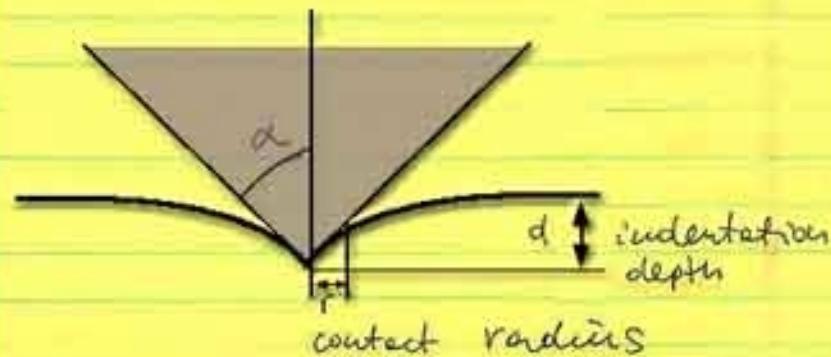
$$F = \frac{2E_1 R}{1-\nu_1^2} d$$

if E_1 and E_2 are comparable

$$F = \frac{2 \cdot R}{\frac{1-\nu_1^2}{E_1} + \frac{1-\nu_2^2}{E_2}} d$$

$$d \sim F$$

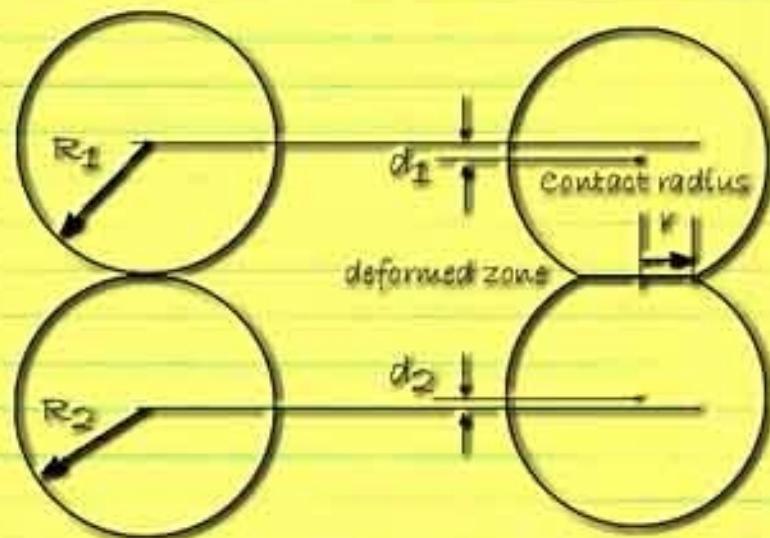
Conical indenter



$$F = \tan \alpha \frac{2E}{\pi(1-\nu^2)} d^2$$

$$d \sim F^{1/2}$$

Sphere - sphere contact (Hertz)



$$d = d_1 + d_2 \quad \text{total deformation}$$

$$K_1 = \frac{1-V_1^2}{E_1} \quad K_2 = \frac{1-V_2^2}{E_2}$$

$$K_{\text{eff}} = K_1 + K_2$$

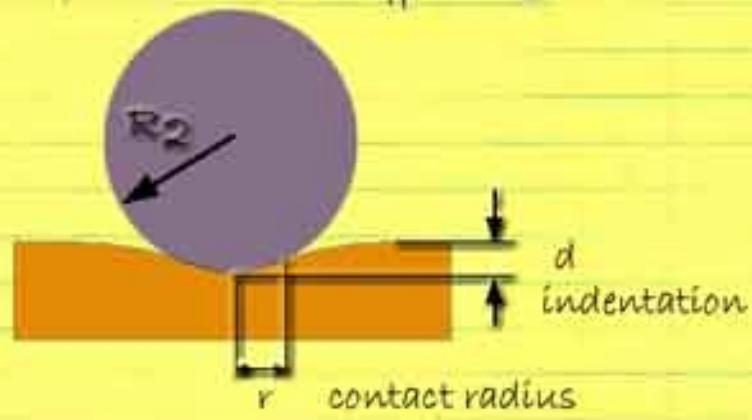
$$R_{\text{eff}} = \frac{R_1 R_2}{R_1 + R_2}$$

contact radius:

$$r^3 = \frac{3\pi}{4} R_{\text{eff}} K_{\text{eff}} \cdot F$$

$$d = \frac{r^2}{R_{\text{eff}}}$$

$$\text{if } R_1 \rightarrow \infty \quad R_{\text{eff}} = R_2$$



indentation vs load in Hertz model:

$$d^3 = \frac{F^6}{R_{\text{eff}}^3} = \frac{3\pi}{4} \frac{k_{\text{eff}}^2}{R_{\text{eff}}} \cdot F^2$$

$$d \sim F^{2/3}$$

distribution of pressure in contact region

$$P(r, x) = \frac{2r}{\pi^2 k_{\text{eff}} R_{\text{eff}}} \sqrt{1-x^2}$$

where r - contact radius

$$x = \frac{s}{r}$$

normalized
distance
from the center

s - distance
from the
center.

JKR (Johnson-Kendall-Roberts) description
of contact: Indentation + Adhesion

$$r^3 = \frac{3\pi}{4} R_{\text{eff}} K_{\text{eff}} (F + q + \sqrt{q^2 + 2qF})$$

Additional load
due to adhesion

$$q = 3\pi R_{\text{eff}} W_{1,2}$$

$W_{1,2}$ - work of adhesion
if external force $F=0$

$$r_0 = \left(\frac{R_{\text{eff}}}{K_{\text{eff}}} 6\pi W_{1,2} \right)^{1/3}$$

Indentation:

$$d = -\frac{r^2}{R_{\text{eff}}} + \frac{2}{3} \frac{r_0^{3/2}}{R_{\text{eff}}} r^{-1/2}$$

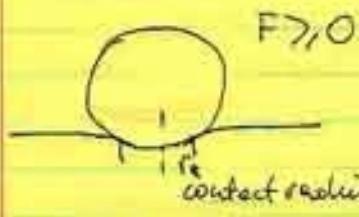
For negative loads ($F < 0$)

contact radius can be still
positive, until

$$\sqrt{q^2 + 2qF} > 0.$$

This means that a neck
connecting the bodies in
contact is formed

Push-in



Pull-out



The force at which the neck breaks can be determined from the condition

$$q_r^2 + 2q_r F_s = 0$$

$$F_s = -\frac{q_r}{2} = -\frac{3}{2} \pi R_{eff} W_{12}$$

Neck radius upon breaking

$$\begin{aligned} r_o^3 &= \frac{3\pi}{4} R_{eff} K_{eff} \left(-\frac{q_r}{2} + q_r \right) = \\ &= \frac{3\pi}{4} R_{eff} K_{eff} \frac{q_r}{2} \end{aligned}$$

$$\text{since } r_o^3 = \frac{3\pi}{4} R_{eff} K_{eff} \cdot 2q_r$$

$$r_s = \frac{r_o}{\sqrt[3]{4}} \approx 0.6 r_o$$

distribution of pressure :

$$P(r, x) = \frac{2 F}{\pi^2 K_{eff} R_{eff}} \sqrt{F x^2} - \frac{\sqrt{\frac{2}{\pi^2} \frac{W_{12}}{K_{eff} \cdot r}}}{\sqrt{F x^2}}$$